# AC Losses and Dielectric Losses in High Temperature Superconducting (HTS) Power Cables for Smart Grid Applications: A Comprehensive Review

Mohit Kalsia\*, Raja Sekhar Dondapati\*\* and Preeti Rao Usurumarti\*\*\*

#### ABSTRACT

High Temperature Superconducting (HTS) cables are being used for effective power transmission and distribution as the losses in these HTS cables are less compared to those in conventional power cables. HTS cable constitutes of BSCCO-2233 or YBCO-123 with critical temperatures 110K at zero Tesla and 90K at zero Tesla respectively are highly opted due to larger handling current carrying capacity. During the operation of HTS cable, receives heat flux from the ambient, AC losses through the superconducting tape, dielectric losses from dielectric material, heat-in-leaks from the current leads.

Hence, it is essential to estimate the losses during the operation of HTS cable. Hence, in the present work, a method of estimating the AC losses during transmission and distribution is presented. Electric probe method and Calorimetric thermal methods are frequently used to measure AC losses. The dielectrical losses are increased due to raise in temperature from the heat fluxes. In this paper, different AC losses and dielectric losses are estimated and methods available in the literature to measure these losses are reviewed.

Keywords: HTS cables; AC losses; Dielectric losses; Calorimeter and Electrical methods ; Dielectric materials.

## 1. INTRODUCTION

High temperature superconducting (HTS) cables are emerging as substitute to next generation power transmission and distribution in power grid applications. These cables not only handle larger currents but also compact and have low losses as compared with conventional cables. Superconductors have zero electrical resistance and conducts electricity with no losses. However, when the alternating current is transmitted through the superconductors, different losses such as AC losses and dielectric losses are [1], [2] encountered. Hence, in designing the HTS cable the factors to be considered are presented in the following sections.

#### 1.1. AC Losses

AC losses comprises of hysteresis losses [1]–[5] in superconducting tapes, eddy current losses [6] in sheath material and coupling losses[5], [6] between the mutlifilaments of HTS tapes. AC losses due to Self field are investigated in detail by Vyas et al [7] and found that the AC losses depend on the transport current. Further, the method of measuring these AC losses by calorimetric method [8], [9], electrical circuit method [9], [10] and contactless electrical measurement [11] are reported in the literature. Moreover, it was reported that the AC losses can be minimized by changing the gaps between the superconducting tapes [12] and reduction in AC losses up to 1.8/W/m/phase is achieved at 5kA [13].

<sup>\*</sup> School of Mechanical Engineering Lovely Professional University, Phagwara, Punjab, India, Email: kalsiamohit.007@gmail.com

<sup>\*\*</sup> School of Mechanical Engineering Lovely Professional University, Phagwara, Punjab, India, Email: drsekhar@ieee.org

<sup>\*\*\*</sup> Department of Mechanical Engineering PVK Institute of Technology Ananthapur, Andhra Pradesh, India, Email: preeti.iitkgp@gmail.com

# 1.2. Dielelectric or tand losses

Based on the dielectrics, HTS cables are classified into warm dielectric and cold dielectric cables. Various dielectric materials used in the HTS cable are Cross Linked Polyethylene (XLPE) [14], and Poly-Propelene Laminated Paper (PPLP) [14]–[17], Kraft paper [17], polyethylene (PE) and PVC. However, PPLP is reported to be suitable material which can withstand electrical breakdown [18]. Moreover, liquid nitrogen  $(LN_2)$  is reported to have suitable dielectric properties which can be used as a coolant [19] in the HTS cable.

# 1.3. Other factors to be considered in design of HTS cables

Thermal losses such as conduction in the corrugated steel pipe, convection losses between the corrugated steel pipe and the cryogenic coolant and heat leaks from the surroundings through the thermal insulation are the other important losses to be considered in the design of HTS Cables. In addition, Mechanical issues such as torsion strain [20], strain tolerance, bending radius, fracture toughness and twist pitch of the HTS cable are mechanical issues to be considered while designing the HTS Cable.

As the losses increase, the critical values of current density, critical field and critical temperature are affected. Hence, it is necessary to investigate on the methods to reduce the losses. Accordingly, cooling strategies are to be implemented to enhance the performance of HTS cables. Few recent works on



Figure 1: Warm dielectric Coaxial cable

Table 1
Experimental, numerical and computational modeling of Superconductors

			AC Losses			Cooling	
		Experimental	Numerical	Computational	Experimental	Numerical	Computational
LTS	Superconducting Magnets	Park [22]	F.Grilli [23]	M.N. Wilson[24] Bottura [25]	Ohya [26]	Marinucci [27] Bottura [28]	R.S. Dondapati [29][30][31]
	Superconducting Cables	Daney [32] Zannella [33] Elschner [34]	Vyas.G [7] Wesche [1]	Grilli [35] Lehtonen [36] Campbell [37]	Mukoyama [38]	Fuchino [39]	R.S.Dondapati [21] Ashworth [40]
	Superconducting Motors	Pei [41] Muta [42]	Malé [43] Nasar [44]	Leveque[45] Fu [46]	Chen [47]	Hong [48]	Yang Kai [49]
	Superconducting Generators	Sakamoto [50]	Magnusson [51] Oberly [52]	Zermeno [53]	Intichar [54]	Jo [55] Abrahamsen [56]	Ries [57]
HTS	Superconducting Fault Current Limiters	Park [58] Agnoux [59]	Otabe [60] Sugita [61]	Song [62]	Yang [63] Kar [64]	Chang [65]	Sousa [66]
	Superconducting Transformers	Ishigohka [67]	Nitta [68] Nab [69]	Formisano [70]	Janu [71]	Chang [72]	Smolka [73]
	Superconducting Magnetic Energy Storage (SMES)	Ohsaki [74]	Xu [75]	Xu[75] Han [76]	Na [77] Ren [78]	R.S.Dondapati [79]	Choi [80]

estimation of AC losses and implementation of cooling strategies with respect to Low Temperature Superconductors (LTS) and High Temperature Superconductor (HTS) devices are compiled in Table 1. Further, a typical view of the single phase warm dielectric HTS cable is shown in Fig. 1. To retain the superconductivity of the HTS tape, Liquid Nitrogen (LN2) is generally used to cool the HTS tape below to its critical temperature [21].

### 2. ESTIAMTION OF LOSSES IN HTS CABLES

## 2.1. AC losses

AC losses can be estimated using the calorimetric and electric circuit methods as follows.

- Calorimetric method: In this method, a Micarta or G-10 [4] tube is used as thermal insulation for the HTS cable. When the current is passed through the current leads connected to HTS cable, generate AC losses and hence induce radial temperature gradient which can be measured using thermocouples. The range of accuracy of measurement depends on the sensitivity of the thermocouples.
- 2) Electrical method: This method is one of the advancements in estimating the AC losses in HTS cables. With the use of digital lock-in amplifier, the angle between the voltage and current signal and the voltage across the cable are measured. If the measured phase angle has a small error, a significant error will arise in AC loss measurement.

The AC losses in the HTS cables are given by [6] as

$$Q_{total} = Q_{self} + Q_{Ba} + Q_{Bc} \tag{1}$$

Where,  $Q_{self} = loss$  due to self field,  $Q_{Ba} = loss$  due to axial field,  $Q_{Bc} = loss$  due to circumferential field According to the Sumitomo's cable

$$Q_{total} = Q_{self} + Q_B (W/m)$$
<sup>(2)</sup>

Where,  $Q_B$  is equal to summation  $Q_{Ba} \& Q_{Bc}$ .

According to Furukawa's cable

$$Q_{total} = Q_B + Q_{self} + Q_{eddy} W/m$$
(3)

As the electrical shielding is not present in this cable, the magnetic fields, the axial field  $B_a$  and the circumferential field  $B_c$  causes eddy current losses. Further, self-field AC losses are calculated by using Norris equation [7] as given by

$$Qac = \frac{\mu_0 I_c^2 f}{\pi} \left[ \left( 1 - \Gamma \right) \ln \left( 1 - \Gamma \right) + \Gamma - \frac{\Gamma^2}{2} \right] (W/m)$$
(4)

$$\Gamma = \frac{I_{pk}}{I_c} \tag{5}$$

For  $\Gamma << 1$ 

$$Qac \simeq \frac{\mu_0 I_c^2 f}{6\pi} \Gamma^3 \tag{6}$$

$$I_{pk} = \sqrt{2}.I_{rms}$$
(7)

$$\Gamma = \frac{\sqrt{2.I_{rms}}}{I_{c,cable}}$$
(8)

$$P = V_{rms} \cdot I_{rms} \cdot \cos\phi \tag{9}$$

where,  $\Gamma$  is the normalized current,  $F_R$  is retention fraction, N is the number of tapes in the cable,  $V_{rms} = RMS$  voltage (V),  $I_{rms} = Transport$  current (A),  $\cos\Phi = power$  factor.

AC losses with the variable transport currents are calculated. As the critical current is increased, AC losses are found to be decreasing as shown in Fig. 2. Further, as the transport current increases, the AC loss is found to be increasing as shown in Fig 3.



Figure 2: AC losses with frequency at various critical currents



Figure 3: AC losses with transport current at various frequencies

#### 2.2. Dielectric losses

The dielectric losses are also called as tand losses. These losses occur when the cryogenic fluid that is supplied could not cool the dielectric material due to the loads such as heat leak from the ambient through the insulation and protective shield.

The dielectric losses per unit length is calculated by [1]

$$P_{d} = 0.5\omega C U_{p}^{2} \tan \delta = \omega U_{p}^{2} \frac{\pi \varepsilon_{0}}{\ln(r_{od}/r_{id})} \varepsilon \tan \delta$$
(10)

where, C is the capacity of cylindrical capacitor and is given by  $C = 2\pi\varepsilon\varepsilon_0 / \ln(r_{od} / r_{id})$  per unit length,  $\omega$  is the angular power frequency given by  $\omega = 2\pi f$ ,  $\varepsilon$  is the dielectric constant of the insulation,  $\varepsilon_0$  is the permittivity of free space, U<sub>p</sub> is phase to ground peak voltage,  $\delta$  is the angle loss,  $r_{od}$  is outer diameter,  $r_{id}$  is inner diameter of the HTS Cable.

The dielectric losses are also calculated by [15] as given by

$$\frac{P_{ins}}{L} \approx S.\omega \int \partial f \,\varepsilon \varepsilon_0 \,\tan \delta E^2 \tag{11}$$

where, S is technical Carnot factor.

#### 3. CONCLUSION

The following conclusions may be drawn from the present review.

- 1) Calorimetric method is slow process. However, it is a straight process. By using this method, AC losses in the range of 0.1W/m to 10W/m were measured.
- 2) Electrical circuit method is quicker and the range of measurment is high when compared with calorimetric method.
- PPLP, XLPE, PE, PVC and krafted paper are used as dielectrics in the warm dielectric (WD) cables. LN2 and PPLP are used as dielectrics in the cold dielectric (CD) cables.
- 4) HTS cables with Direct current (DC) are free from losses as compared to those with Alternating Current (AC). However, DC transmission and storage requires a large equipment which adds to enormous cost. DC transmission is done with the CD cables only.
- 5) The AC losses are also reduced by the methods such as narrow filament diameter, twisting the filaments and introducing barrier between filaments for minimizing the coupling.

#### REFERENCES

- R. Wesche, A. Anghel, B. Jakob, G. Pasztor, and R. Schindler, "Design of superconducting power cables," *Cryogenics* (*Guildf*)., vol. 39, pp. 767–775, 1999.
- [2] J. Oestergaard, J. Okholm, K. Lomholt, and O. Toennesen, "Energy losses of superconducting power transmission cables in the grid," *IEEE Trans. Appl. Supercond.*, vol. I, no. March, pp. 2–5, 2001.
- [3] V. V Zubko, A. A. Nosov, N. V Polyakova, S. S. Fetisov, and V. V Vysotsky, "Hysteresis Loss in Power Cables Made of 2G HTS Wires With NiW Alloy Substrate," *IEEE Trans. Appl. Supercond.*, vol. 21, no. 3, pp. 988–990, 2011.
- [4] J. W. Lue, J. A. Demko, L. Dresner, R. L. Hughe, U. Sinha, J. C. Tolbert, and S. Co, "AC Losses of Prototype HTS Transmission Cables," *IEEE Trans. Appl. Supercond.*, vol. 9, no. 2, pp. 416–419, 1999.
- [5] S. S. Fetisov, V. V Zubko, A. A. Nosov, N. V Polyakova, and V. S. Vysotsky, "Losses in Power Cables Made of 2G HTS Wires with Different Substrates," *Phys. Procedia*, vol. 36, pp. 1319–1323, 2012.

- [6] S. S. J. Šouc and F. G. P. Kovac, "Experimentally Determined Magnetization ac Losses of Mono and Multifilamentary MgB 2 Wires," J Supercond NovMagn, vol. 26, pp. 1557–1561, 2013.
- [7] G. Vyas, R. S. Dondapati, and P. R. Usurumarti, "Parametric Evaluation of AC Losses in 500 MVA/1.1 kA High Temperature Superconducting (HTS) Cable for Efficient Power Transmission: Self Field Analysis," *Model. Symp. (EMS), 2014 Eur.*, pp. 315–319, 2014.
- [8] H. Noji, K. Ikeda, K. Uto, and T. Hamada, "Calculation of the total AC loss of high- T C superconducting transmission cable," *Phys. C*, vol. 448, pp. 1066–1068, 2006.
- [9] D. E. Daney, "Single-phase AC losses in prototype HTS conductors for superconducting power transmission lines," *Phys. C SUPER Conduct.*, vol. 310, pp. 236–239, 1998.
- [10] H. Noji, "Numerical analysis of the AC losses of 500-m HTS power cable in Super-ACE project," Cryog. 47, vol. 47, pp. 94–100, 2007.
- [11] C. Træholt and E. Veje, "Contactless electrical measurements of transport ac losses in a 3 m long superconducting cable," Supercond. Sci. Technol., vol. 898, pp. 2–6, 2002.
- [12] Y. Kito, O. Tsukamoto, and S. Fukui, "AC Transport Current Loss of High Temperature Superconducting Tapes in Single Layer Arrangements," Int. Conf. Magn. Technol., pp. 1214–1217, 1997.
- [13] M. Ohya, T. Masuda, N. Amemiya, A. Ishiyama, and T. Ohkuma, "Development of 66 kV class REBCO superconducting cable," *Phys. Procedia*, vol. 27, pp. 364–367, 2012.
- [14] J. Choi, J. Choi, H. Kim, J. Cho, S. Kim, and A. High-temperature, "Manufacture and Insulating Test of a Mini-Model," *IEEE Trans. Appl. Supercond.*, vol. 19, no. 3, pp. 1789–1792, 2009.
- [15] S. Mukoyama, M. Yagi, N. Fujiwara, and H. Ichikawa, "Conceptual design of 275 kV class high-Tc superconducting cable," *Phys. C Supercond. its Appl.*, vol. 470, no. 20, pp. 1563–1566, 2010.
- [16] Y. Kim, D. Kwag, H. Kim, J. Cho, K. Seong, and S. Kim, "Research on Insulation Design of 22 . 9-kV High- T c Superconducting Cable in Korea," *IEEE Trans. POWER Deliv.*, vol. 20, no. 2, pp. 554–559, 2005.
- [17] D. S. Kwag, V. D. Nguyen, S. M. Baek, H. J. Kim, J. W. Cho, and S. H. Kim, "A Study on the Composite Dielectric Properties for an HTS Cable," *IEEE Trans. Appl. Supercond.*, vol. 15, no. 2, pp. 1731–1734, 2005.
- [18] W. J. Kim, H. J. Kim, J. W. Cho, and S. H. Kim, "The basic properties of PPLP for HTS DC cable," *Phys. Procedia*, vol. 45, pp. 293–296, 2013.
- [19] C. Sumereder, "Dielectric measurements on HTS insulation systems for electric power equipment," *Phys. C*, vol. 386, pp. 411–414, 2003.
- [20] M. Takayasu, J. V Minervini, and L. Bromberg, "Torsion Strain Effects on Critical Currents of Hts Superconducting Tapes," AIP Conf. Proc., vol. 1219, pp. 337–344, 2010.
- [21] R. S. Dondapati and V. V Rao, "Pressure Drop and Heat Transfer Analysis of Long Length Internally Cooled HTS Cables," in *Applied Superconductivity, IEEE Transactions on*, 2013, vol. 23, no. 3, p. 5400604.
- [22] J. Park, S. Kim, I. Park, and S. Jeong, "Experimental investigation of AC loss in a conduction-cooled layer-wound (RE) BCO magnet for continuous Adiabatic Demagnetization Refrigerator (ADR)," *Cryogenics (Guildf).*, vol. 63, pp. 77–84, 2014.
- [23] F. Grilli, V. M. R. Zermeño, and M. Takayasu, "Numerical modeling of twisted stacked tape cables for magnet applications," *Phys. C Supercond. its Appl.*, vol. 518, pp. 122–125, Nov. 2015.
- [24] M. N. Wilson, "Stabilization of superconducting magnet systems," Cryogenics (Guildf)., vol. 18, no. 9, p. 571, Sep. 1978.
- [25] L. Bottura, P. Bruzzone, J. B. Lister, C. Marinucci, and A. Portone, "Computations of AC loss in the ITER magnets during fast field transients," *IEEE Trans. Appl. Supercond.*, vol. 17, pp. 2438–2441, 2007.
- [26] M. Ohya, a. Higuchi, Y. Shirai, M. Shiotsu, and S. Imagawa, "Cooling stability test of He II cooled LHD conductor (2) -Experimental results," *IEEE Trans. Appl. Supercond.*, vol. 14, no. 2, pp. 1447–1450, 2004.
- [27] C. Marinucci, L. Bottura, and P. Bruzzone, "Transient stability analysis of the SeCRETS experiment in SULTAN," *IEEE Trans. Appl. Supercond.*, vol. 12, no. 1, pp. 1524–1527, 2002.
- [28] L. Bottura, C. Marinucci, and P. Bruzzone, "Application of the code THEA to the CONDOPT experiment in SULTAN," *IEEE Trans. Appl. Supercond.*, vol. 12, no. 1, pp. 1528–1532, 2002.
- [29] D. Raja Sekhar and V. V. Rao, "Three dimensional CFD analysis of Cable-in-Conduit Conductors (CICCs) using porous medium approach," *Cryogenics (Guildf)*., vol. 54, pp. 20–29, Feb. 2013.
- [30] R. S. Dondapati and V. V. Rao, "Entropy generation minimization (EGM) to optimize mass flow rate in dual channel cablein-conduit conductors (CICCs) used for fusion grade magnets," *Fusion Eng. Des.*, vol. 89, no. 6, pp. 837–846, Jun. 2014.

- [31] R. S. Dondapati and V. V. Rao, "Influence of mass flow rate on Turbulent Kinetic Energy (TKE) distribution in Cable-in-Conduit Conductors (CICCs) used for fusion grade magnets," *Fusion Eng. Des.*, vol. 88, no. 5, pp. 341–349, Jun. 2013.
- [32] D. E. Daney, H. J. Boenig, M. P. Maley, and S. Fleshler, "Calorimeter for measuring AC losses in HTS cables for superconducting power transmission lines," *Cryogenics (Guildf)*., vol. 39, pp. 225–233, 1999.
- [33] S. Zannella, L. Montelatici, G. Grenci, M. Pojer, L. Jansak, M. Majoros, G. Coletta, R. Mele, R. Tebano, and F. Zanovello, "AC Losses in Transport Current Regime in Applied AC Magnetic Field/ : Experimental Analysis and Modeling," *IEEE Trans Appl. Supercond.*, vol. I, no. I, pp. 1–4, 2001.
- [34] S. Elschner, E. Demencik, B. Douine, F. Grilli, A. Kudymow, M. Stemmle, S. Strauss, V. Zermeno, and W. Goldacker, "New Experimental Method for Investigating AC Losses in Concentric HTS Power Cables," *IEEE Trans. Appl. Supercond.*, vol. 25, no. 3, pp. 1–5, 2015.
- [35] F. Grilli, F. Sirois, S. Member, M. Laforest, and S. P. Ashworth, "Periodic Space-Time Formulation for Numerical AC Loss Computation in Superconductors," *IEEE Trans. Appl. Supercond.*, vol. 19, no. 3, pp. 3565–3568, 2009.
- [36] J. Lehtonen, J. Paasi, and R. Mikkonen, "Computation of losses in a HTS tape carrying AC transport current in external AC magnetic field at temperatures of 20-40 K," *IEEE Trans. Appl. Supercond.*, vol. 3, no. 7, pp. 11–14, 2000.
- [37] A. M. Campbell, "An Introduction to Numerical Methods in Superconductors," J Supercond NovMagn, vol. 24, pp. 27–33, 2011.
- [38] S. Mukoyama, M. Yagi, M. Ichikawa, S. Torii, T. Takahashi, H. Suzuki, and K. Yasuda, "Experimental results of a 500 m HTS power cable field test," *IEEE Trans. Appl. Supercond.*, vol. 17, no. 2, pp. 1680–1683, 2007.
- [39] S. Fuchino, M. Furuse, and N. Higuchi, "Longitudinal Temperature Distribution in Superconducting Power Cables with," *IEEE Trans. Appl. Supercond.*, vol. 12, no. 1, pp. 1339–1342, 2002.
- [40] S. P. Ashworth and D. W. Reagor, "A novel cooling scheme for superconducting power cables," *Cryogenics (Guildf)*., vol. 51, no. 4, pp. 161–167, 2011.
- [41] R. Pei, A. Velichko, M. Majoros, Y. Jiang, R. Viznichenko, Z. Hong, R. Marchant, a M. Campbell, and T. a Coombs, "\$I\_C\$ and AC loss of 2G YBCO tape measurement for designing and fabrication of an HTS motor," *IEEE Trans. Appl. Supercond.*, vol. 18, no. 2, pp. 1236–1239, 2008.
- [42] I. Muta, H. J. Jung, T. Hirata, T. Nakamura, T. Hoshino, and T. Konishi, "Fundamental experiments of axial-type BSCCObulk superconducting motor model," *IEEE Trans. Appl. Supercond.*, vol. 11, no. I, pp. 1964–1967, 2001.
- [43] G. Malé, T. Lubin, S. Mezani, and J. Lévêque, "Analytical calculation of the flux density distribution in a superconducting reluctance machine with HTS bulks rotor," *Math. Comput. Simul.*, vol. 90, pp. 230–243, 2013.
- [44] S. a. Nasar, G. Y. Xiong, and Z. X. Fu, "Eddy-current losses in a tubular linear induction motor," *IEEE Trans. Magn.*, vol. 30, no. 4, pp. 1437–1445, 1994.
- [45] J. Leveque, D. Netter, B. Douine, and A. Rezzoug, "Some considerations about the cooling of the rotor of a superconducting motor," *IEEE Trans. Appl. Supercond.*, vol. 17, no. 1, pp. 44–51, 2007.
- [46] W. N. Fu and S. L. Ho, "Dynamic Demagnetization Computation of Permanent Magnet Motors Using Finite Element Method With Normal Magnetization Curves," *IEEE Trans. Appl. Supercond.*, vol. 20, no. 3, pp. 851–855, 2010.
- [47] A. Chen, X. Liu, F. Xu, J. Cao, and L. Li, "Design of the cryogenic system for a 400 kW experimental HTS synchronous motor," *IEEE Trans. Appl. Supercond.*, vol. 20, no. 3, pp. 2062–2065, 2010.
- [48] Z. Hong, Y. Jiang, R. Pei, W. Yuan, R. Marchant, and T. A. Coombs, "Numerical Analysis of the Demagnetization Effect in a Superconducting Machine With Bulk HTS Material on the Rotor," *IEEE Trans. Appl. Supercond.*, vol. 19, no. 3, pp. 2897–2900, 2009.
- [49] K. Yang and F. Yaojing, "Design of Novel Spiral Magnetic Poles and Axial-Cooling Structure of Outer-Rotor PM Torque Motor," *Ieee Trans. Appl. Supercond.*, vol. 20, no. 3, pp. 838–841, 2010.
- [50] O. Sakamoto, T. Nakano, T. Nitta, H. Kameda, T. Kumano, M. Asada, and A. Izumi, "Theoretical and experimental study on characteristics of slow response type superconducting generator for high harmonic armature current," *IEEE Trans. Appl. Supercond.*, vol. 14, no. 2, pp. 892–895, 2004.
- [51] N. Magnusson, A. B. Abrahamsen, D. Liu, M. Runde, and H. Polinder, "Hysteresis losses in MgB 2 superconductors exposed to combinations of low AC and high DC magnetic fields and transport currents," *Phys. C SUPER Conduct.*, pp. 1–5, 2014.
- [52] C. E. Oberly, L. Long, G. L. Rhoads, and W. J. Carr, "ac Loss analysis for superconducting generator armatures wound with subdivided Y ± Ba ± Cu ± O coated tape," vol. 41, 2001.
- [53] V. M. R. Zermeno, B. Abrahamsen, N. Mijatovic, B. B. Jensen, and N. F. Pedersen, "Simulation of an HTS Synchronous Superconducting Generator," *Phys. Proceedia*, vol. 36, pp. 786–790, 2012.

- [54] L. Intichar and C. Schnapper, "Experimental Simulation of a Helium Cooling System for a Superconducting Generator," *Le J. Phys. Colloq.*, vol. 45, no. 1, pp. C1–729–C1–732, 1984.
- [55] Y. S. Jo, J. P. Hong, J. Lee, Y. K. Kwon, and K. S. Ryu, "Approach to the shape optimum design of superconducting synchronous generator," *IEEE Trans. Appl. Supercond.*, vol. 10, pp. 939–942, 2000.
- [56] A. B. Abrahamsen, B. B. Jensen, E. Seiler, N. Mijatovic, V. M. Rodriguez-zermeno, N. H. Andersen, and J. Østergård, "Feasibility study of 5 MW superconducting wind turbine generator," *Phys. C Supercond. its Appl.*, vol. 471, no. 21–22, pp. 1464–1469, 2011.
- [57] Gn. experiments on helium flow in superconducting generators Ries, "Numerical experiments on helium flow in superconducting generators," *IEEE Trans. Magn.*, vol. 24, no. 2, pp. 1485–1488, 1988.
- [58] D. K. Park, J. S. Bang, S. E. Yang, T. K. Ko, Y. S. Yoon, M. C. Ahn, and K. Sim, "Theoretical and Experimental Analysis of AC Loss Characteristic of Bifilar Pancake Coil With Coated Conductor," *IEEE Trans. Appl. Supercond.*, vol. 18, no. 2, pp. 1232–1235, 2008.
- [59] C. Agnoux and C. Cottevieille, "EXPERIMENTAL 7.2 kVrms/l kArmJ3 kAp,,k CURRENT LIMITER SYSTEM," IEEE Trans. Appl. Supercond., vol. 3, no. 1, 1993.
- [60] E. S. Otabe, M. Migita, M. Watanabe, T. Matsushita, and M. Morita, "Numerical analysis of AC current loss in QMG fault current limiter by finite element method," *Phys. C Supercond.*, vol. 382, no. 1, pp. 127–131, Oct. 2002.
- [61] S. Sugita and H. Ohsaki, "Numerical analysis of AC losses in REBCO thin film for coated conductor and fault current limiter," *Phys. C Supercond.*, vol. 392–396, P, pp. 1150–1155, Oct. 2003.
- [62] M. Song, Y. Tang, J. Li, Y. Zhou, L. Chen, and L. Ren, "Thermal analysis of HTS air-core transformer used in voltage compensation type active SFCL," *Phys. C Supercond. its Appl.*, vol. 470, no. 3, pp. 1657–1661, 2010.
- [63] S. E. Yang, M. C. Ahn, D. K. Park, K. S. Chang, B. Seok, H. Chang, J. Park, and T. K. Ko, "Experimental Method for Determining the Recovery of Superconducting Fault Current Limiter Using Coated Conductor in a Power System," *IEEE Trans. Appl. Supercond.*, vol. 18, no. 2, pp. 652–655, 2008.
- [64] S. Kar, S. Kulkarni, S. K. Sarangi, and V. V. Rao, "Conceptual design of a 440 V/800 a resistive-type superconducting fault current limiter based on high T c coated conductors," *IEEE Trans. Appl. Supercond.*, vol. 22, no. 5, 2012.
- [65] H.-M. C. H.-M. Chang, G. H. L. G. H. Lee, J. S. J. Sim, K.-B. P. K.-B. Park, I.-S. O. I.-S. Oh, J.-B. S. J.-B. Song, and H. L. H. Lee, "Two-Stage Cryocooling Design for Hybrid Superconducting Fault Current Limiter," *IEEE Trans. Appl. Supercond.*, vol. 20, no. 3, pp. 2047–2050, 2010.
- [66] W. T. B. De Sousa, A. Polasek, R. Dias, C. F. T. Matt, and R. D. A. Jr, "Thermal electrical analogy for simulations of superconducting fault current limiters," *Cryogenics (Guildf).*, vol. 62, pp. 97–109, 2014.
- [67] T. Ishigohka, K. Uno, and S. Nishimiya, "Experimental Study on Effect of In-Rush Current of Superconducting Transformer," *IEEE Trans. Appiled Supercond.*, vol. 16, no. 2, pp. 1473–1476, 2006.
- [68] T. Nitta, "Some considerations on superconducting transformers from a design-point of view," *IEEE Trans. Magn.*, vol. 32, no. 4, pp. 2381–2384, 1996.
- [69] W. Nab, J. Joo, and G. S. Cha, "Analytic Approaches to Quench Behaviours of Superconducting Transformer," Int. Conf. Magn. Technol., pp. 575–578, 1997.
- [70] A. Formisano, F. Marignetti, R. Martone, G. Masullo, A. Matrone, R. Quarantiello, and M. Scarano, "Performance Evaluation for a HTS Transformer.," *IEEE Trans. Appl. Supercond.*, vol. 16, no. 2, pp. 1501–1504, 2006.
- [71] Z. Janu and J. Wild, "Experimental setup for precise measurement of losses in high-temperature superconducting transformer," *Cryogenics (Guildf)*., vol. 46, pp. 759–761, 2006.
- [72] H.-M. Chang, Y. S. Choi, S. W. Van Sciver, and K. D. Choi, "Cryogenic cooling system of HTS transformers by natural convection of subcooled liquid nitrogen," *Cryogenics (Guildf)*., vol. 43, pp. 589–596, 2003.
- [73] J. Smolka, "CFD-based 3-D optimization of the mutual coil con fi guration for the effective cooling of an electrical transformer," *Appl. Therm. Eng.*, vol. 50, no. 1, pp. 124–133, 2013.
- [74] H. Ohsaki, S. Taniguchi, S. Nagaya, S. Akita, S. Koso, and M. Tatsuta, "Development of SMES for power system control: Present status and perspective," *Phys. C Supercond. its Appl.*, vol. 412–414, no. 2, pp. 1198–1205, 2004.
- [75] Y. Xu, Y. Tang, L. Ren, F. Jiao, M. Song, K. Cao, D. Wang, L. Wang, and H. Dong, "Distribution of AC loss in a HTS magnet for SMES with different operating conditions," vol. 494, pp. 213–216, 2013.
- [76] P. Han, Y. Wu, H. Liu, L. Li, and H. Yang, "Structural Design and Analysis of a 150 kJ HTS SMES Cryogenic System," *Phys. Procedia*, vol. 67, pp. 360–366, 2015.
- [77] J. B. Na, H. Kang, Y. J. Hwang, S. E. Yang, D. K. Park, D. K. Bae, and T. K. Ko, "Experimental study on the electrical

breakdown characteristics of sub-cooled liquid nitrogen for designing a high voltage superconducting machine," *IEEE Trans. Appl. Supercond.*, vol. 20, no. 3, pp. 1662–1666, 2010.

- [78] L. Ren, Y. Tang, J. Li, Z. Li, L. Chen, J. Chen, J. Shi, and J. Wen, "Conduction-cooled YBCO HTS current lead for SMES application," *IEEE Trans. Appl. Supercond.*, vol. 20, no. 3, pp. 1737–1740, 2010.
- [79] A. A. Sarkar and R. S. Dondapati, "A novel approach to estimate the thermophysical properties of pure oxygen at the supercritical region to be used in SMES," pp. 67–74, 2015.
- [80] J. H. Choi, H. G. Cheon, J. W. Choi, H. J. Kim, K. C. Seong, and S. H. Kim, "A study on insulation characteristics according to cooling methods of the HTS SMES," *Phys. C Supercond. its Appl.*, vol. 470, no. 20, pp. 1703–1706, 2010.